

## THE SEPARATION OF ADDITIVELY OVERLAPPING TG STEPS BY NON-LINEAR OPTIMIZATION

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### ABSTRACT

A method for the kinetic analysis of overlapping reactions is described. Typical reactions of dehydration are used to demonstrate the procedure.

### INTRODUCTION

The experiences hitherto acquired in the kinetic analysis of non-isothermal experiments show that the kinetic parameters obtained by the known procedures in general do not describe the experimental curve in an optimum manner. In particular, this is true of overlapping reactions. The reasons for this are discussed and investigations have shown that the sources of errors can partly be eliminated /1/. By applying a non-linear optimization method to TG and DTG data a better fit of the theoretical conversion curve to the experimental one could be obtained.

### RESULTS AND DISCUSSION

Typical dehydration reactions characterized by a single reaction step were studied to demonstrate this method with specially prepared  $Mg(OH)_2$  /3/, natural halloysite and chlorite, a four-sheet silicate, having been used for the studies. These experiments were carried out by the use of the Mettler thermoanalyzer TA 1. The results of the kinetic analysis in the evaluation intervals cited are shown in Table 1. The relative error of E is found to be  $\pm 5\%$ . It can be seen that, independently of the selected interval of the conversion curve, constant parameters are obtained. This fact proves the reaction to be a single-step one. If overlapping occurs, the parameters change by describing the conversion curve by intervals. This is demonstrated, for example, with china clay (Table 2).

Table 1. Kinetic parameters for single-step reactions

Substance	Range (K)	Parameters		
		E (kJ/mol)	n	WL (%)
Mg(OH) <sub>2</sub>	620 - 730	192,2	0,8	29,6
	640 - 730	191,8	0,8	29,6
	660 - 730	202,4	0,8	29,0
	680 - 730	202,6	0,8	29,7
	640 - 710	187,7	0,7	29,6
	660 - 710	199,9	0,8	29,0
Halloysite	700 - 860	146,3	0,6	11,7
	700 - 850	144,1	0,6	11,8
	720 - 850	145,6	0,6	11,8
	740 - 850	145,1	0,6	11,8
	760 - 850	148,3	0,6	11,8
Chlorite	800 - 1010	187,2	1,0	9,9
	850 - 990	178,7	1,0	9,8
	820 - 1010	185,5	1,1	9,9

Table 2. Kinetic parameters for various intervals of china clay

Range (K)	Parameters		
	E(kJ/mol)	n	WL (%)
750 - 835	176,2	1,2	10,6
750 - 845	179,1	1,4	10,5
760 - 845	176,4	1,3	10,6
770 - 845	171,3	1,2	10,8
750 - 855	178,8	1,4	10,7
750 - 865	179,7	1,4	10,5
750 - 870	181,8	1,4	10,4
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750 - 890	193,9	1,7	11,3
750 - 900	198,2	1,8	11,5
750 - 910	204,5	2,0	12,6
750 - 920	216,9	2,2	12,7

The procedure as represented is the prerequisite to the description of additively overlapping reactions. With carbon-containing clay, as an example, two reaction steps are revealed by determining the kinetic parameters in intervals (Fig. 1). The step obtained with the clay investigated in the range of 700 to 760 K corresponds to the step of dehydroxylation of the kaolinite. The content of double-sheet silicate in the clay can be determined from the separated weight step with high accuracy. The reaction step located in front of the dehydroxylation can be described in an optimum manner by the use of the parameters cited, having to be ascribed to the oxidation of the carbon contained in the clay (humic acids). The reaction step in the final range corresponding to the difference curve between the two calculated weight steps

and the experimental curve is caused by the dehydroxylation of non-distinguishable three-sheet clay minerals. Their content can be determined from the difference between the total weight loss and the calculated weight steps.

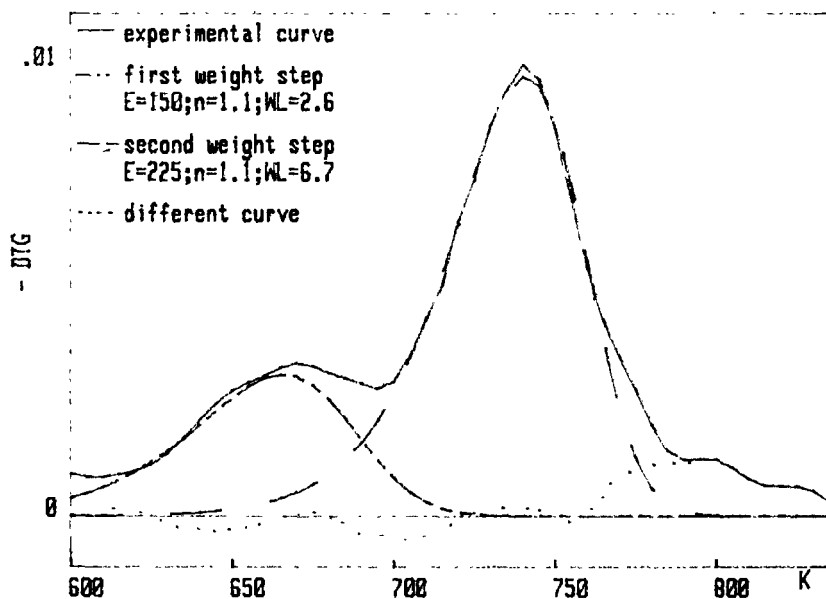


Fig.1. Model curve as calculated for carbon-containing clay

The investigation into the thermal decomposition of mixed carbonate ( $\text{CaCO}_3 + \text{SrCO}_3$ ) shows that two overlapping decomposition steps occur. The kinetic analysis gives the following result (Table 3).

For the first reaction step from 940 to 1050 K the kinetic parameters remain constant as the evaluation interval varies. When the interval is extended up to higher temperatures, the effect of overlapping becomes evident from the variation of the parameters. By subtraction of the model curve (calculated with  $E = 205,7$ ;  $n = 0,8$ ) we obtain an overlapping-free second reaction step which, in turn, can be optimized similarly to a single-step reaction.

Table 3. Kinetic parameters of the decomposition of mixed carbonate

Range (K)	Parameters		
	E (kJ/mol)	n	WL (%)
940 - 1050	205,9	0,8	17,2
960 - 1050	205,0	0,8	17,2
980 - 1050	205,4	0,8	17,2
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960 - 1060	217,2	0,9	17,0
960 - 1070	231,4	1,0	17,0
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1140 - 1260	262,1	0,35	20,3
1170 - 1260	262,1	0,35	20,3
1120 - 1260	262,1	0,35	20,3

The thermal analysis of bauxite, in general, indicates several overlapped dehydration steps of the hydrated oxides contained. For the exemple studied we were able to describe two reaction steps by kinetic analysis. The first ( $E = 286,2$ ;  $n = 1,3$ ;  $WL = 34,1$  %) corresponds to the dehydration of hydrargillite, the second ( $E = 175,0$ ;  $n = 1,4$ ;  $WL = 19,2$  %) to that of alumogoethite. For the identification by phase analysis one has to take into consideration that the dehydration temperature is highly affected by the degree of disorder of the hydroxides.

#### CONCLUSIONS

The results show the kinetic analysis of overlapping reaction steps by non-linear optimization of the TG and DTG curves to be possible. The prerequisite to the application of this method, however, ist the existence of an overlapping-free partial interval in at least one reaction step. From the partial weight losses obtained quantitative statements as to the phase composition of mineral mixtures can be made.

#### REFERENCES

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